

Hail impact damage on PV modules

Presented by:

James Hartley, Sandia National Laboratories Team:

Jennifer Braid (SNL); Colin Sillerud (CFV Labs)

DuraMAT Webinar, December 18, 2023









SAND2023-146160

CFV Labs

- Introduction to the problem
- Current practices for testing modules vs. hail
 - Development and remaining limitations
- DuraMAT research: Simulating hail vs. PV module impacts
 - Ice ball and PV module models
 - Experimental validation efforts
- Various insights on hail vs. PV modules
 - Combined experimental and simulated analyses

INREL





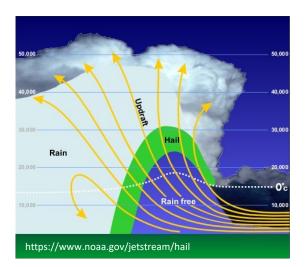


Introduction to the problem

- In general terms: Hail is solid precipitation which forms due to updrafts within clouds
 - Growth continues while updraft is able to sustain the mass
 - Begins to fall when mass becomes excessive or conditions shift
- May take on a wide array of shapes and sizes



Examples of natural hailstones



Weather conditions favoring hail formation

CFV Labs

Dura MAT

INREL





Introduction to the problem

- Hard ice balls + glass PV modules = bad (expensive) outcomes
 - Subcritical damage is also bad for long term performance



Hail damage affects both residential and commercial deployments. Apparently undamaged modules may degrade at higher rates

Dura MAT

្ឋNREL

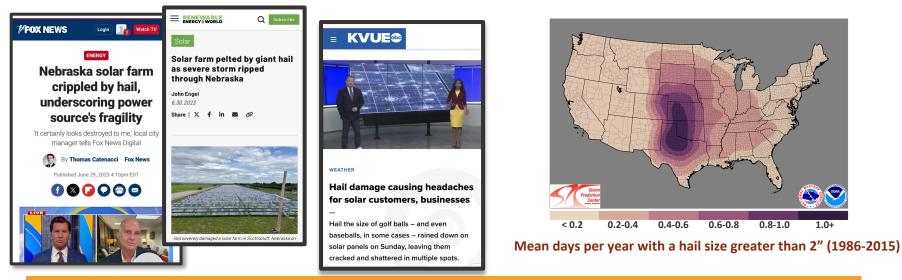






Introduction to the problem

- Nowhere is 100% safe, especially with increasing module life expectancies
- Even when hail does not happen: Insurance costs and reputation risk are damaging to PV adoption



Understanding hail damage potential is crucial for informed decision making

()Dura**MAT**

SNREL





CFV Labs

- Introduction to the problem
- Current practices for testing modules vs. hail
 - Development and remaining limitations
- DuraMAT research: Simulating hail vs. PV module impacts
 - Ice ball and PV module models
 - Experimental validation efforts
- Various insights on hail vs. PV modules
 - Combined experimental and simulated analyses

INREL







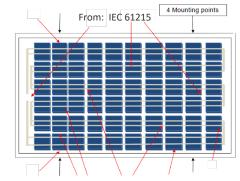
Current practices for testing PV modules vs. hail

- Qualification tests attempt to replicate the impact event with ball drops (since deprecated) or projected ice balls (current practice)
 - Most prevalent is IEC 61215 (with various historical equivalents from ASTM, NIST, UL..)
- Tests specify a sequence of impacts at certain locations on the module, at increasing ice ball sizes until failure
- "Pass" certification is given at the largest size where the module survived the full sequence









Standard impact locations for testing

CFV I ahs

DuraMAT

SNREL





Current practices for testing PV modules vs. hail

- Tests are based on replicating the kinetic energy of falling hail at terminal velocity
 - At terminal velocity: Gravitational force matches aerodynamic drag force
 - Kinetic energy: Amount of energy associated with a moving mass and velocity

Gravitational force Drag force

Variable

ρ U

 C_D

A

q

m

$$F_g = mg$$

$$F_D = \frac{1}{2}\rho U^2 C_D A$$

Value

1.18 kg/m³, typical

20-50 m/s

~0.5 for a sphere, typical

 πr^2 , r is radius of ice ball

9.81 m/s², for Earth

Ice volume times ice density

| Kinetic Energy | $E = \frac{1}{2}mU^2$ |
|----------------|-----------------------|
|----------------|-----------------------|

| | Diameter Mass | | Test velocity | Kinetic energy | |
|-----|---------------|------|---------------|----------------|--|
| | mm | g | m/s | J | |
| | 25 | 7,53 | 23,0 | 2,0 | |
| | 30 | 14,0 | 25,1 | 4,1 | |
| les | 35 | 20,7 | 27,2 | 7,7 | |
| re | 40 | 32,3 | 29,0 | 12,9 | |

Hail diameter and velocity parameters from IEC Module Qualification Test #17, Hail Test

2

Definition

Density of air

Velocity in air

Drag coefficient

Frontal area

Gravity constant

Mass of ice ball

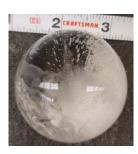


Most modul



Limitations of current test practices

- Test ice balls are carefully controlled but are not real hail
 - As specified: Optically clear, free from cracks, spherical, prescribed velocity
 - Real hail: Extremely variable on density, drag coefficient (hence velocity)
 - Large emphasis on kinetic energy alone
 - Impact mechanics are a function of materials too





A standard ice ball used for testing vs. natural hailstone examples

Dura**MAT**

CINREL

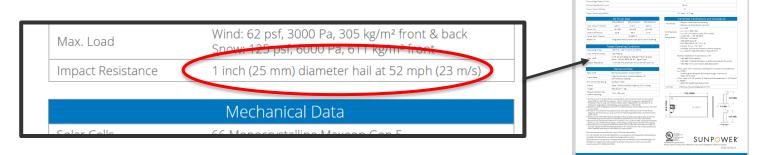






Limitations of current test practices

- Qualification tests produces very little differentiation between modules
 - Pass criteria based on major defects and safety only
 - No effective measure of margins
 - Some independent test labs have developed sequential sequences for impact + aging
 - PVEL: Hail Stress Sequence (HSS)
 - RETC: Hail Durability Test (HDT)
- Expensive and time consuming to perform tests



A typical 25 mm hail certification as appearing on a module datasheet

©NREI

ura**MAT**







- Introduction to the problem
- Current practices for testing modules vs. hail
 - Development and remaining limitations

• DuraMAT research: Simulating hail vs. PV module impacts

- Ice ball and PV module models
- Experimental validation efforts
- Various insights on hail vs. PV modules
 - Combined experimental and simulated analyses

INREL

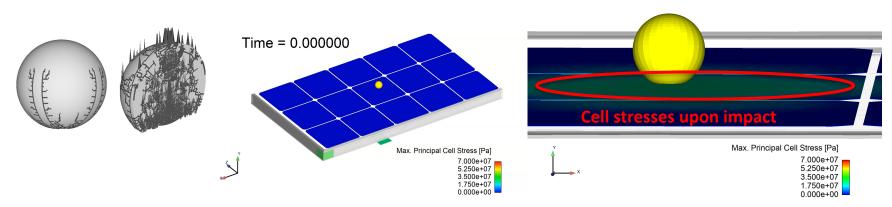






Current research within DuraMAT: Analyzing Hail Impacts using Computational Simulation

- Simulating the hail impact event using finite element analysis methods allows it to be analyzed in full detail: glass or cell stresses as a function of module design, impact parameters, etc.
 - Hail (ice) material model: Exists in literature and previously implemented at Sandia
 - Module model: Previously developed under DuraMAT 1 projects



Hail vs. PV module simulations allow the full impact sequence to be analyzed in detail

C.I. Hammetter, R.L. Jones, H.L. Stauffacher, T.F. Schoenherr, "Measurement and modeling of supersonic hailstone impacts", International Journal of Impact Engineering, Volume 99, 2017, Pages 48-57, ISSN 0734-743X, https://doi.org/10.1016/j.ijimpeng.2016.09.001





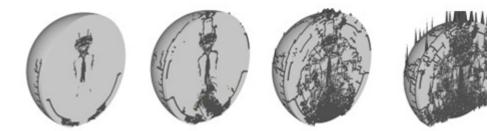




CFV Lahs

Validating the hail ice material model

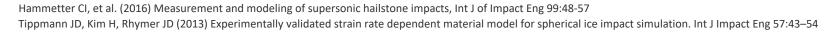
- Simulated ice ball must deliver the correct force vs. time profile to the module
- To validate: measure an impact and compare to simulated expectation
 - High frequency (50 kHz) load cell for direct measurement of impact forces vs. time



Simulated ice material failure progression during an impact

CINREL

IraMAT

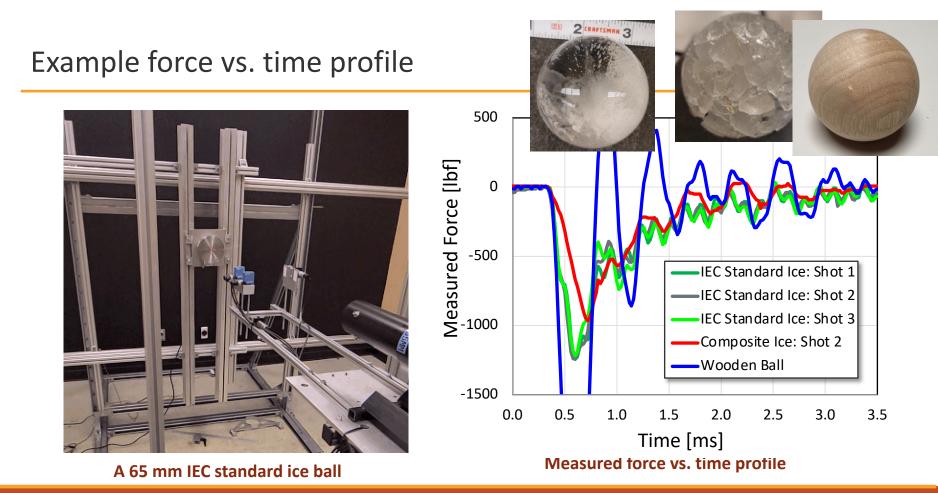








CEV Labs



DuraMAT

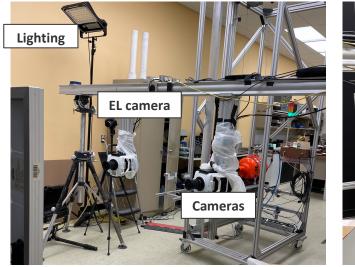




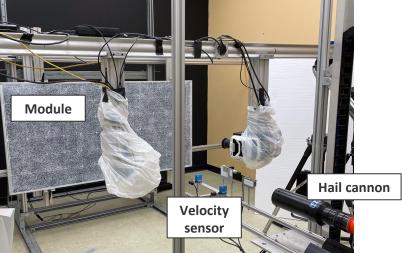
CFV Labs

Validating the simulation: Module dynamic response

- Stereo high speed video of a hail impact was recorded for analysis with digital image correlation (DIC) to process module deflections vs. time
- Matching dynamic response to simulations provides confidence in model applicability



Test setup: Module view



Test setup: Cannon view

DuraMAT

SNREL

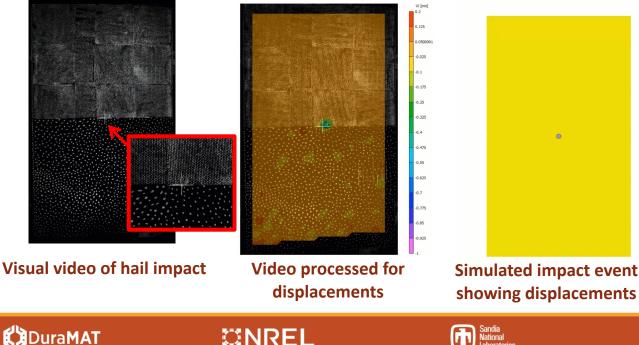


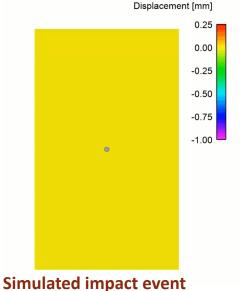


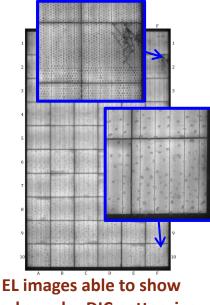


Module dynamic response comparisons

- Experimental technique has been verified to be applicable to most modules
- Measurement resolution of <0.1 mm spatially, 100 μ s temporally .







cracks under DIC patterning



- Introduction to the problem
- Current practices for testing modules vs. hail
 - Development and remaining limitations
- DuraMAT research: Simulating hail vs. PV module impacts
 - Ice ball and PV module models
 - Experimental validation efforts
- Various insights on hail vs. PV modules
 - Combined experimental and simulated analyses

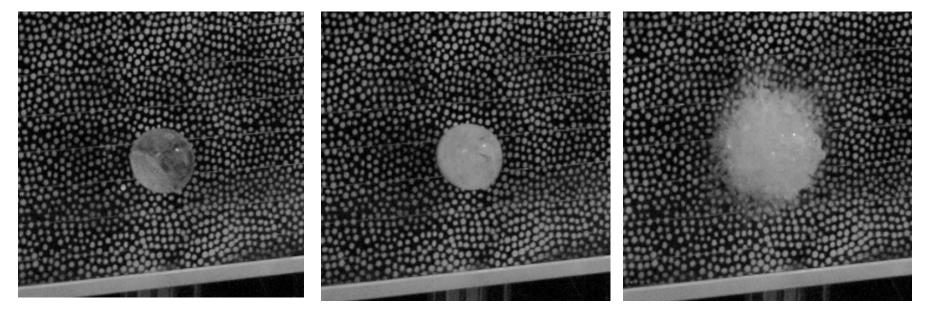
INREL







• Initial contact (t = 0) to 100 μ s: Ice ball shatters



Video frames showing ice ball initial contact and shattering. Frame rate: 11,000 Hz

Dura MAT

SNREL







~40 to ~300 µs: Stress in backside of glass reaches maximum

©NRE|

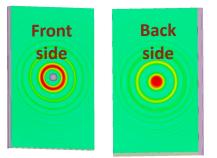
Ice failure flag

1st Princ. Stress [Pa]

ura**MAT**

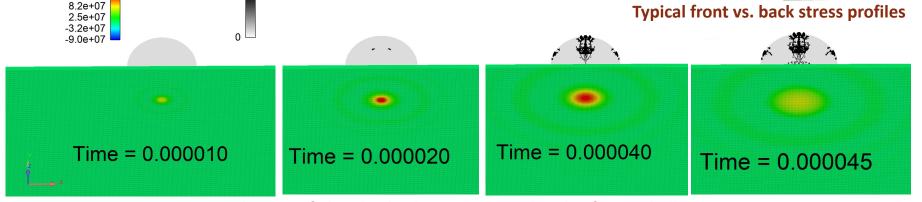
1.4e+08

- Timing and magnitude are sensitive to modeled ice behavior
- Dissipation is extremely rapid once maximum is reached
- Local spot of tensile stress on glass backside, ring on front side



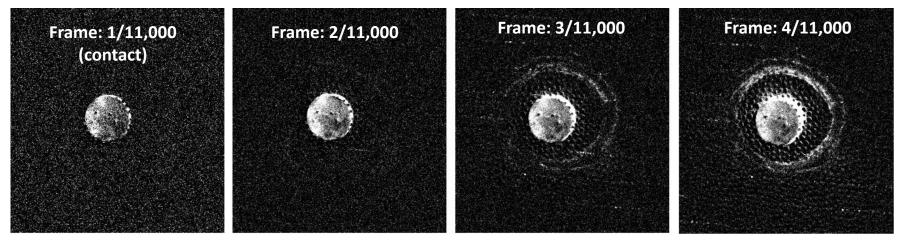


CFV Labs



Simulations of glass backside stress immediately after ice ball contact

- ~100-300 μs: Glass failure initiates (when present)
 - Of interest for further study- current frame rate and visibility near ball are less definitive



Sequential video frame image differences showing appearance of glass fracture by +300 μ s

🗱 Dura MAT

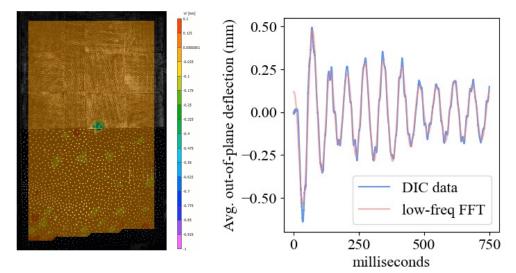
SNREL





CFV Labs

- 300 µs to 2 seconds: Module oscillates and returns to resting state
 - Key frequencies are identifiable, ~11.5 Hz and 14.4 Hz for a 60-cell module



Deformations vs. time on a 60 cell module, visualized and processed by average out of plane movement

🕻 🕽 Dura MAT

CNREL

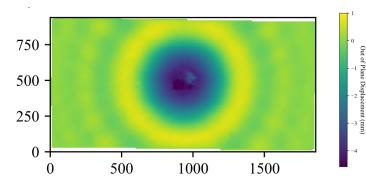






Modules are much tougher than their qualification level implies (for isolated impacts)

- Most modules will survive 55 mm standardized ice impacts at normal incidence over homogeneous glass area
- Lower qualification levels of ~35 mm are due to failures from specific locations
 - Junction boxes and edges are special vulnerabilities



Deformation profile for a 55 mm ice impact after 3 ms



Test results on module face from ice ball testing (glass-backsheet shown)

CFV Lahs

🕻 Dura MA1

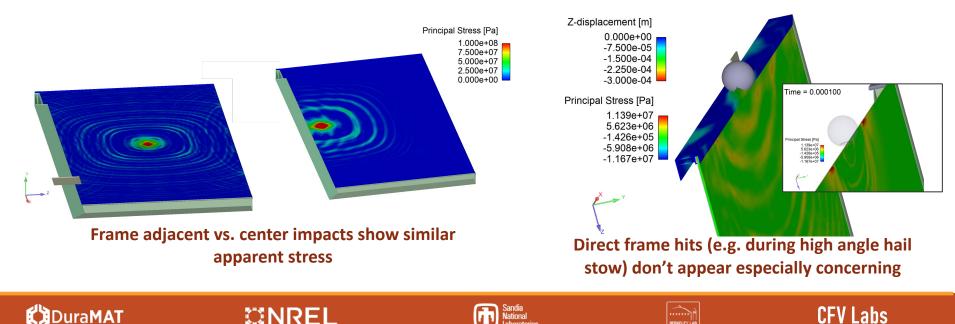
୍କ INREL





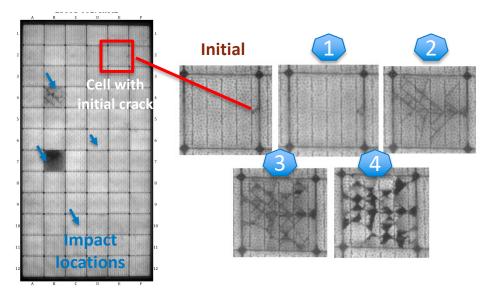
Why do frame-adjacent impacts carry a higher failure probability?

- Stresses within the glass are similar for frame adjacent vs. center area impacts
 - Mechanism appears to be crack initiation from the weaker glass edge, not necessarily an increase in stress due to the applied constraint

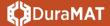


Cell cracks are VERY readily propagated by impacts...

• If an initial cell crack was present at all in the module, propagation occurred with EVERY subsequent impact



Sequential crack propagation at a cell away from actual impacts











Cell cracks are VERY readily propagated by impacts...



Post-impact stress profiles places sufficient stress on remote cells to open cracks



_ ∷NREL







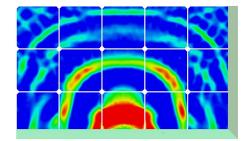
... but cell cracks are not particularly easy to initiate with impact

- For **both** glass-glass and glass-backsheet packaging: Cell cracks were seldom achievable ۲ without also breaking the glass
 - Glass and cell failure thresholds overlap
 - Initial cell and lamination quality appears to be more influential than packaging type
 - Modeled cell stresses are not obviously over established crack criteria _

| BOM | Modules | Total Shots | [New] Cell crack observations | Glass failure observations | Principal Stress [f 1.000e+ 7.500e+ |
|---------------------|---------|----------------|----------------------------------|-------------------------------|---|
| Glass- Glass | 8 | 72 | 8 | 8 | 5.000e+ 2.500e+ 0.000e+ |
| Glass- Backsheet | 8 | 97 | 6 | 7 | Simula |

Results of a hail test suite of 150+ impacts

Pal +08 +07 +07 +07 +00



CFV Labs

ted cell stresses during a probable glass failure are near cracking threshold

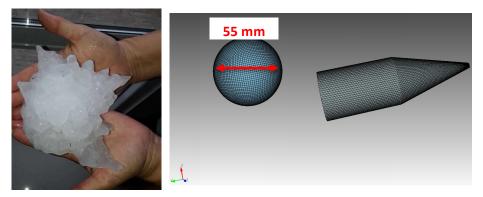
ura**MAT**



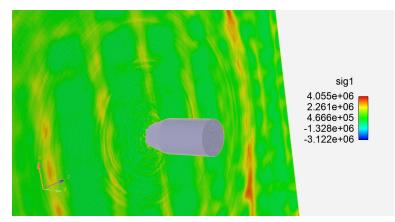


Ice shape has a secondary effect on damage potential

- Hail ice often assumes unusual shapes including sharp points
- Is a point-first impact significantly more damaging?
 - Ice material strength appears insufficient to create major stress concentrations



Approximating a worst-case ice shape. Energy parameters are 55 mm spherical equivalent



Stress profile induced by a worst-case pointed ice ball is not significantly worse than a spherical case

CEV Labs

🗱 Dura MAT

SNREL





- Hail vs. PV modules is an active area of research- much is known but much more to understand
- Computational simulations can add data to augment field observations and explain phenomena
 - Many additional cases may be simulated, to best understand trends and mechanisms
- By fully understanding the problem, optimal decisions can be made around module deployment, design, and insurance











James Y. Hartley Sandia National Laboratories jkyuan@sandia.gov

Jen Braid Sandia National Laboratories jlbraid@sandia.gov

Colin Sillerud CFV Labs colin.sillerud@cfvlabs.com

Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525

SAND2023-146160

ura**MAT**







